# ME 471: Turbulent Combustion, Spring 2012 <br> Stanford University <br> Homework 2: Review of turbulent flows (II) and Premixed Turbulent Combustion (I) <br> Due Tuesday, May 8 in class. 

Guidelines: Please turn in a neat and clean homework that gives all the formulae that you have used as well as details that are required for the grader to understand your solution. Show all work. Required plots should be generated using computer software such as Matlab or similar program. Answers should be written in the blank spaces provided in these homework sheets. Use the back of the page in case you need additional space (not recommended to use more space than provided), for which a clear indication should be written to warn the reader of the presence of text there. Vector quantities are denoted in bold letters in what follows.

Student's Name:
Student's ID:

Solve either Question 1 or Question 2, and solve Problem 1.
Question 1 ( 50 pts )
a) Obtain a relation between the Favre average $\widetilde{\phi}$ and the Reynolds average $\bar{\phi}$ for a scalar field $\phi=\phi(\mathbf{x}, t)$. Why is Favre averaging used in formulations of turbulent combustion?
b) Derive a transport equation for the scalar variance $\widetilde{\phi^{\prime \prime}}$. To do this, follow these steps: First derive a transport equation for $\widetilde{\phi^{2}}$, and then obtain another transport equation for $(\widetilde{\phi})^{2}$. Then use the relation $\widetilde{\phi^{\prime \prime 2}}=\widetilde{\phi^{2}}-(\widetilde{\phi})^{2}$ to obtain the transport equation for the scalar variance (use back of the page for more space). Also, give a brief description of each of the different terms in your equation.

## Student's Name:

## Question 2 (50 pts)

Select true (T) or false (F) for each of the statements in the list provided for each question. A complementary and brief mathematical proof / sketch of your answer on the back of the page would be welcome, but it is not needed in order to get full credit.
2.1 In turbulent flows at high Reynolds numbers,
a) the maximum kinetic energy is located within the Kolmogorov range (T/F)
b) the viscous dissipation generated by the motion of the large eddies is much larger than the turbulent dissipation (T/F)
c) the large scales have turnover times which are much faster than the turnover time of the Kolmogorov eddies (T/F)
d) large-eddy simulations resolve all scales in the flow up to a maximum wave number beyond which physical subgrid-scale models may (or may not) be employed (T/F).
2.2 In a turbulent flow carrying a scalar $\phi$ with a single integral length scale $\ell=\ell_{\phi}$, characteristic large-eddy turnover velocity $u^{\prime}$, molecular diffusivity $D$, and Schmidt number $\mathrm{Sc}=\nu / D$,
a) molecular diffusion of the scalar takes place at the integral scale $\ell$; this is why the turbulent diffusivity $D_{t}$ is usually defined by relations of the type $u^{\prime} \ell / D_{t}=O(1)(\mathrm{T} / \mathrm{F})$
b) there is no molecular diffusion in turbulent flows because in the asymptotic limit of infinite Reynolds numbers $u^{\prime} \ell / D \rightarrow \infty$ the Euler equations are recovered; this is why computing turbulent reacting flows becomes so much more straightforward than computing laminar reacting flows (T/F)
c) molecular diffusion of the scalar $\phi$ takes place at scales of the same order as the Batchelor scale, $\ell_{B}=\mathrm{Sc}^{-1 / 2} \ell_{k}$, where $\ell_{k}$ is the Kolmogorov scale (T/F)
d) the Reynolds number based on the turbulent diffusivity $D_{t}$, (i.e. $u^{\prime} \ell / D_{t}$ ) is typically much larger than the Reynolds number based on the molecular diffusivity $D$, (i.e. $\left.u^{\prime} \ell / D\right)(\mathrm{T} / \mathrm{F})$.
2.3 In the mixing of two reactants in a turbulent flow,
a) the scalar dissipation rate is always a sink in the scalar variance equation (T/F)
b) the scalar dissipation rate indicates zones where molecular mixing is taking place (T/F)
c) the scalar dissipation rate is maximum in zones where only one of the reactants exists ( $\mathrm{T} / \mathrm{F}$ )
d) the scalar dissipation of interest for turbulent combustion is defined as the Reynolds-average of the turbulent diffusivity multiplied by the square of the gradient of the scalar fluctuations (neglecting density variations) (T/F)
e) for order-unity Schmidt numbers, the molecular mixing of two reactants typically occurs in time scales which are much faster than the integral time scale (T/F)
f) macroscopic mixing or stirring is sufficient for having chemical reaction between both reactants (T/F).

## Problem 1 (50 pts)

A cylindrical premixed burner in a power plant is designed to burn a stoichiometric mixture of gaseous methane $\left(\mathrm{CH}_{4}\right)$ and air in a chamber pressurized at 20 bar. A sketch of the burner is shown below. Just upstream of the combustor intake, the $\mathrm{CH}_{4}$ - air feed stream has been passed through a grid to promote turbulence, in such a way that a streamwise turbulent intensity $15 \%$ and an approximate integral length scale 3 cm are obtained. a) Give an estimate of the resolution requirements required for the direct numerical simulation of this burner in terms of the total number of grid points $N$, the minimum grid spacing $\Delta x$ (make the assumptions that you most like regarding grid topology), the minimum time step $\Delta t$ and the total number of time steps $N_{t}$ (assume an explicit fully-compressible code). b) Based on the premixed turbulent-combustion diagram explained in class, characterize the combustion regime in which this burner is likely to be operating. (Note: In case you need additional data, you can use external references but make sure you cite them below)


Figure 1: Sketch of the burner. In this figure, $2 a$ denotes the diameter of the burner and $L$ its axial length. The dashed line represents the boundaries of the computational domain.

