SEPT 23

ASSIGNMENT

READ SECTION 5.1 PAGE 125-138

HOMEWORK 1 DUE SEPT 30

TODAY'S TOPICS

SIMPLE DESCRIPTION OF EXCITATION

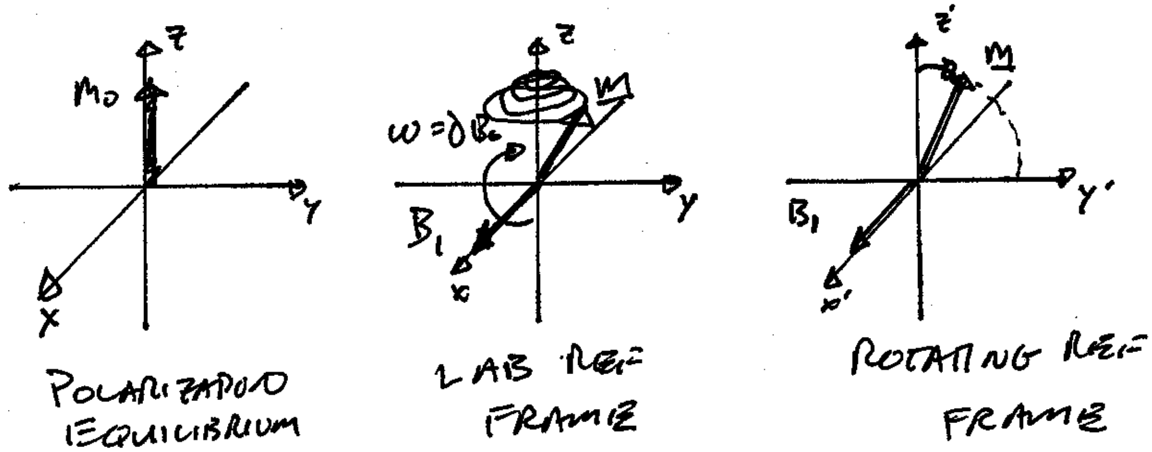
BLOCH EQUATION NEGLECTING T_1, T_2

SMALL TIP ANGLE SOLUTION

EXCITATION K-SPACE

SLICE-SELECTIVE FOURIER DESIGN

SIMPLE DESCRIPTION OF EXCITATION



MOTION OF THE MAGNETIZATION DESCRIBED BY THE <u>BLOCH EQUATION</u>

BLOCH EQUATION INCLUDING RELAXATION

$$\frac{d}{dt}\begin{pmatrix} m_x \\ m_y \\ m_z \end{pmatrix} = \begin{pmatrix} -1/T_2 & \gamma \underline{G}\cdot\underline{r} & -\gamma B_{1,y} \\ -\gamma \underline{G}\cdot\underline{r} & -1/T_2 & \gamma B_{1,x} \\ \gamma B_{1,y} & -\gamma B_{1,x} & -1/T_1 \end{pmatrix}\begin{pmatrix} m_x \\ m_y \\ m_z \end{pmatrix} + M_0 \begin{pmatrix} 0 \\ 0 \\ \frac{1}{T_1} \end{pmatrix}$$

WHERE

$\underline{G} = (G_x, G_y, G_z)$ GRADIENTS ($\underline{G}(t)$)

$\underline{r} = (x, y, z)$ POSITION

FOR MOST OF THIS COURSE, WE WILL IGNORE T_1, T_2. EXCITATION IS FAST COMPARED TO RELAXATION.

BLOCH EQUATION NEGLECTING RELAXATION

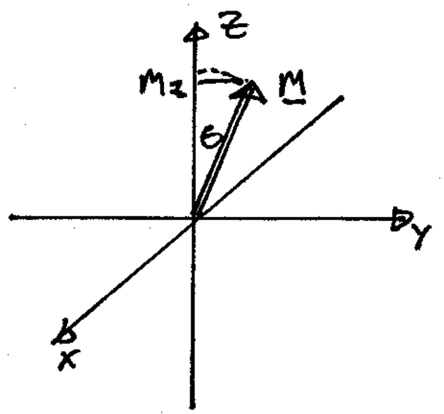
$$\frac{1}{T_1}, \frac{1}{T_2} \sim 0$$

$$\frac{d}{dt}\begin{pmatrix} M_x \\ M_y \\ M_z \end{pmatrix} = \begin{pmatrix} 0 & \gamma \underline{G}\cdot\underline{r} & -\gamma B_{1,y} \\ -\gamma \underline{G}\cdot\underline{r} & 0 & \gamma B_{1,x} \\ \gamma B_{1,y} & -\gamma B_{1,x} & 0 \end{pmatrix}\begin{pmatrix} M_x \\ M_y \\ M_z \end{pmatrix}$$

THE SOLUTION TO THIS EQUATION IS A ROTATION

WE WILL RETURN TO THIS IN 2 WEEKS!

SMALL-TIP-ANGLE APPROXIMATION



FLIP ANGLE θ SMALL MEANS

$$M_z \simeq M_0$$

FIRST TWO EQUATIONS DECOUPLE

$$\frac{d}{dt} M_x = 0 + \gamma \underline{G}\cdot\underline{r} M_y - \gamma B_{1,y} M_0$$

$$\frac{d}{dt} M_y = -\gamma \underline{G}\cdot\underline{r} M_x + 0 + \gamma B_{1,x} M_0$$

COMBINE THESE INTO A SINGLE EQN

DEFINE

$$m_{xy} = m_x + i\, m_y \qquad (m_{xy}(\underline{r}, t))$$

$$B_1 = B_{1,x} + i\, B_{1,y} \qquad (B_1(t))$$

MULTIPLY THE SECOND ($\frac{d}{dt} m_y$) EQUATION BY i, AND ADD THE TWO

$$\frac{d}{dt}(m_x + i m_y) = \gamma \underline{G} \cdot \underline{r}\, m_y - \gamma B_{1,y} m_0 - i \gamma \underline{G} \cdot \underline{r}\, m_x + i \gamma B_{1,x} m_0$$

$$= \gamma \underline{G} \cdot \underline{r}\, (m_y - i m_x) + \gamma m_0 (-B_{1,y} + i B_{1,x})$$

$$= \gamma \underline{G} \cdot \underline{r}\, (-i^2 m_y - i m_x) + \gamma m_0 (i^2 B_{1,y} + i B_{1,x})$$

$$= \gamma \underline{G} \cdot \underline{r}\, (-i)(m_x + i m_y) + \gamma m_0 (i)(B_{1,x} + i B_{1,y})$$

$$\frac{d}{dt} m_{xy} = -i \gamma \underline{G} \cdot \underline{r}\, m_{xy} + i\, m_0 \gamma B_1$$

$$\frac{d}{dt} m_{xy}(\underline{r}, t) = -i \gamma \underline{G}(t) \cdot \underline{r}\, m_{xy}(\underline{r}, t) + i\, m_0 \gamma B_1(t)$$

$$\frac{d}{dt} m_{xy}(\underline{r}, t) + i \gamma \underline{G}(t) \cdot \underline{r}\, m_{xy}(\underline{r}, t) = i\, m_0 \gamma B_1(t)$$

SIMPLE 1ST ORDER DIFFERENTIAL EQN

SOLVE USING INTEGRATING FACTOR

MULTIPLY BOTH SIDES BY

$$e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}$$

PRODUCING

$$m_{xy}(\underline{r},t)\, e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds} + i\gamma\, \underline{G}(t)\cdot\underline{r}\; m_{xy}(\underline{r},t)\, e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}$$
$$= i\gamma m_0 B_1(t)\, e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}$$

THE LEFT SIDE IS NOW AN EXACT DERIVATIVE

$$\frac{d}{dt}\left[m_{xy}(\underline{r},t)\, e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}\right]$$
$$= i\gamma m_0 B_1(t)\, e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}$$

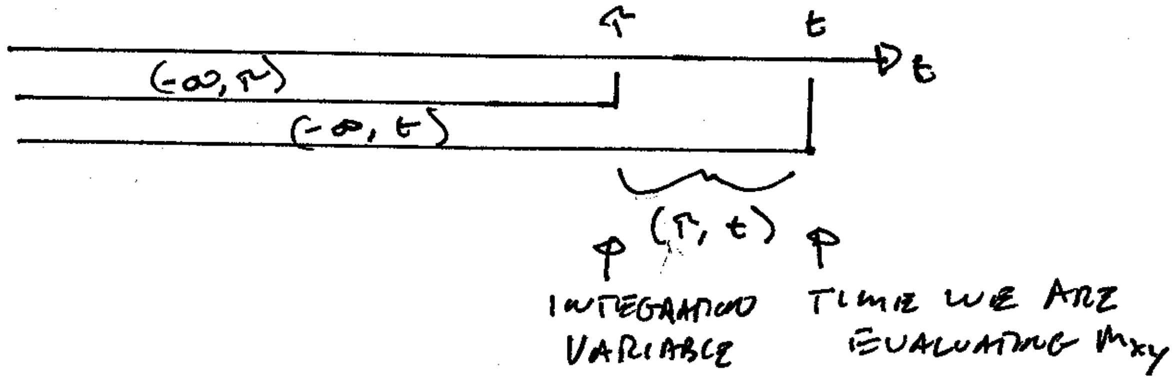
INTEGRATING BOTH SIDES

$$m_{xy}(\underline{r},t)\, e^{i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds} = i m_0 \int_{-\infty}^{t} \gamma B_1(\tau)\, e^{i\int_{-\infty}^{\tau} \gamma \underline{G}(s)\cdot \underline{r}\, ds}\, d\tau$$

$$m_{xy}(\underline{r},t) = i m_0\, e^{-i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds} \int_{-\infty}^{t} \gamma B_1(\tau)\, e^{i\int_{-\infty}^{\tau} \gamma \underline{G}(s)\cdot \underline{r}\, ds}\, d\tau$$

$$= i m_0 \int_{-\infty}^{t} \gamma B_1(\tau)\, e^{-i\int_{-\infty}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}\, e^{+i\int_{-\infty}^{\tau} \gamma \underline{G}(s)\cdot \underline{r}\, ds}\, d\tau$$

LIMITS ON THE ARGUMENTS OF EXPONENTIALS



COMBINING EXPONENTIALS

$$\underline{m_{xy}(\underline{r}, t) = i m_0 \int_{-\infty}^{t} \gamma B_1(\tau)\, e^{-i\int_{\tau}^{t} \gamma \underline{G}(s)\cdot \underline{r}\, ds}\, d\tau}$$

THIS IS IN THE FORM OF A FOURIER TRANSFORM

K-SPACE FORMULATION

DEFINE

$$\underline{k}(\tau, t) = -\frac{\gamma}{2\pi} \int_{\tau}^{t} \underline{G}(s)\, ds$$

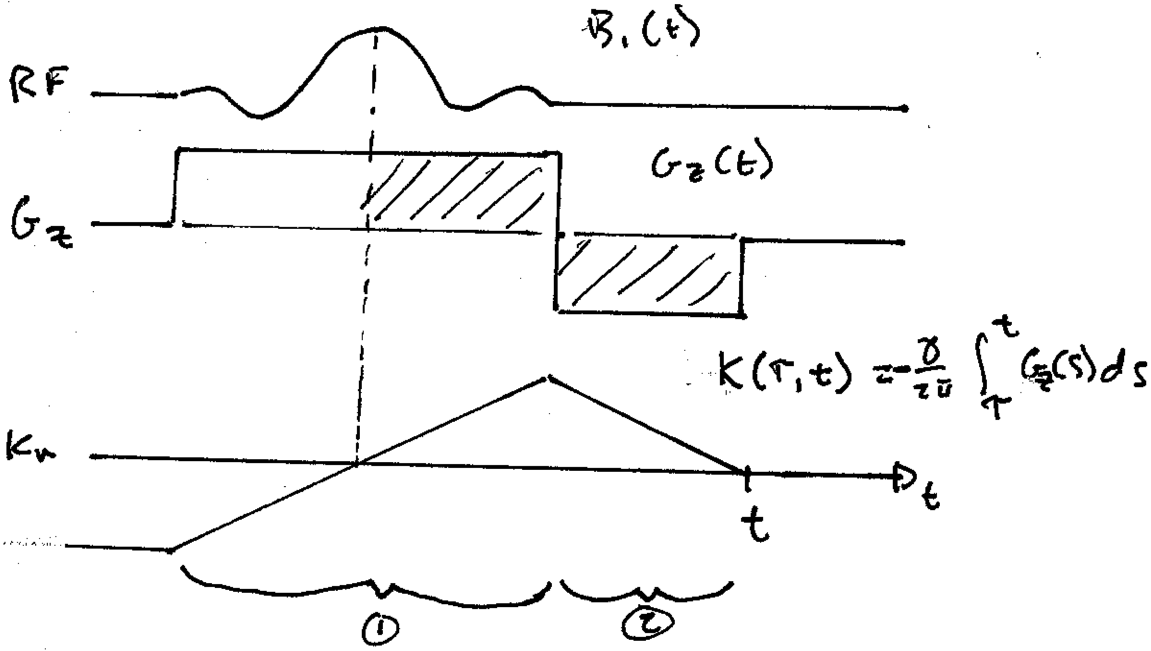
(INTEGRAL OF REMAINING GRADIENT)

DIFFERENT FROM READOUT, CONVENTION FOR EXCITATION
"EXCITATION" K-SPACE

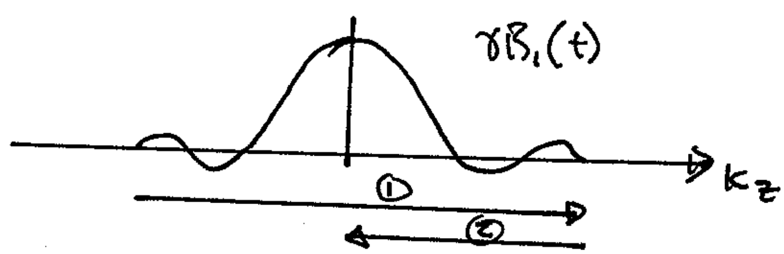
THEN

$$\underline{m_{xy}(\underline{r}, t) = i m_0 \int_{-\infty}^{t} \gamma B_1(\tau)\, e^{i 2\pi \underline{k}(\tau, t)\cdot \underline{r}}\, d\tau}$$

EXAMPLE: SLICE SELECTION



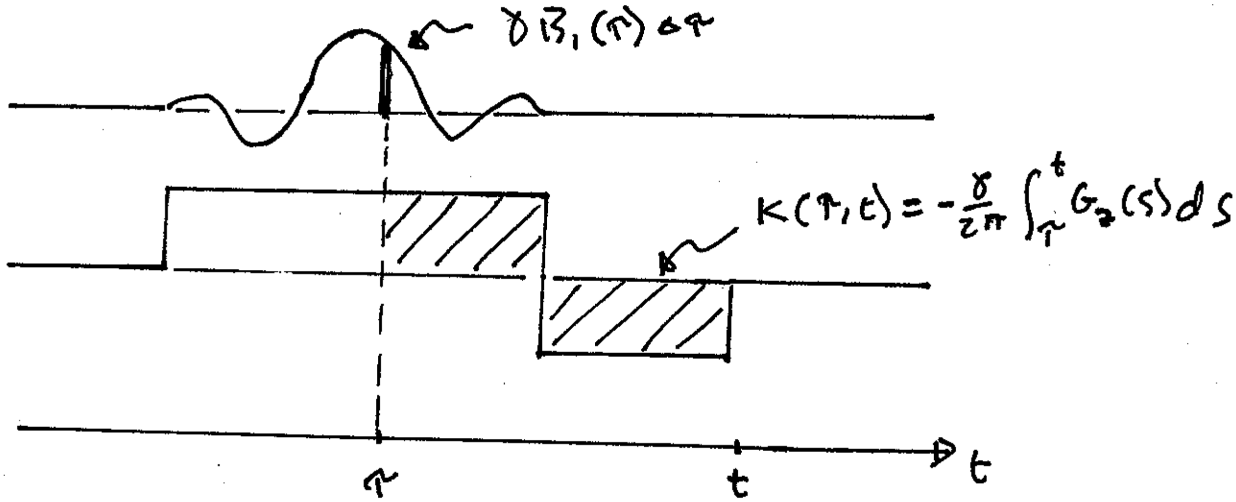
RF APPLIES A WEIGHTING IN K-SPACE DURING ①



THE REFOCUSING LOBE ② SHIFTS THE WEIGHTING BACK TO THE MIDDLE

REFOCUSES THE SLICE

GRAPHICAL DERIVATION



SMALL INCREMENT IN EXCITATION

$$\gamma B_1(\tau)\Delta\tau$$

PRODUCES SMALL INCREMENT IN MAGNETIZATION

$$\Delta m_{xy} = (\gamma B_1(\tau)\Delta\tau)(i m_0)$$

THIS PRECESSES BY

$$k(\tau,t) = -\frac{\gamma}{2\pi}\int_\tau^t G_z(s)\,ds$$

TO PRODUCE A PHASE

$$e^{i2\pi k(\tau,t) z}$$

MAGNETIZATION FROM THIS INCREMENT AT END OF PULSE

$$(i m_0)\,\gamma B_1(\tau)\Delta\tau\, e^{i2\pi k(\tau,t) z}$$

INTEGRATE OVER ALL SUCH INCREMENTS

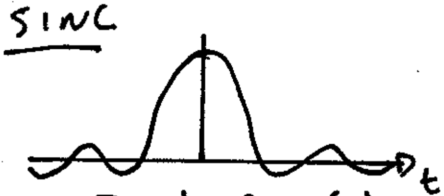
$$m_{xy}(z,t) = i M_0 \int_{-\infty}^{t} \gamma B_1(\tau) e^{i 2\pi k(\tau,t) z} \, d\tau$$

FOURIER DESIGN OF SLICE SELECTIVE PULSES

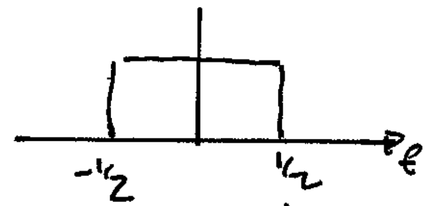
SLICE PROFILE IS FOURIER TRANSFORM OF RF PULSE, K-SPACE WEIGHTING.

CHOOSE AN RF PULSE WITH NICE TRANSFORM

SINC



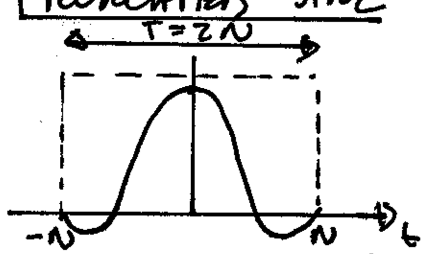
$B_1(t) = \mathrm{sinc}(t)$



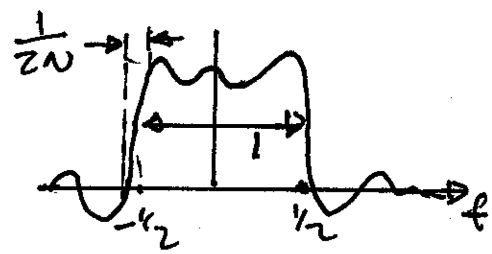
$\mathrm{rect}(f)$

NOT PRACTICAL, SINCE $\mathrm{sinc}(\cdot)$ CONTINUES INDEFINITELY

TRUNCATED SINC



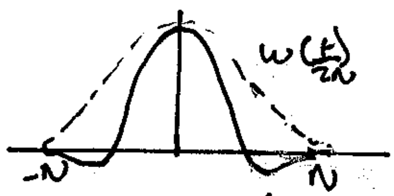
$\mathrm{sinc}(t)\,\mathrm{rect}\left(\frac{t}{2N}\right)$



$\mathrm{rect}(f) * 2N\,\mathrm{sinc}(2Nf)$

TOO MUCH RIPPLE

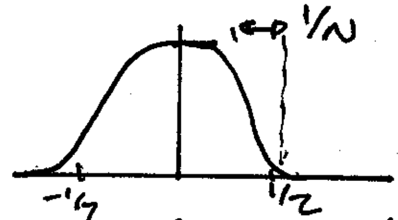
WINDOWED SINC



$\mathrm{sinc}(t)\,w\left(\frac{t}{2N}\right)$

$w(t)$ HAMMING WINDOW

JUST RIGHT!



$\mathrm{rect}(f) * 2N\,W(2Nf)$

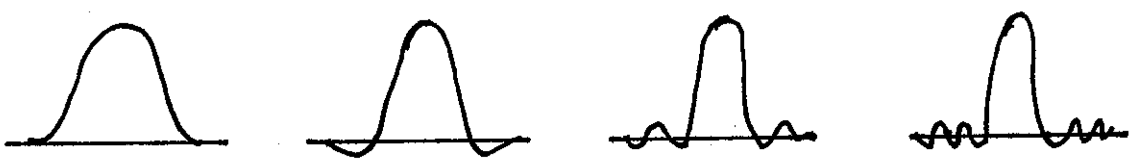
CHARACTERIZATION OF PULSE SHAPE

TIME - BANDWIDTH PRODUCT

$$TBW = (2N)\,1$$

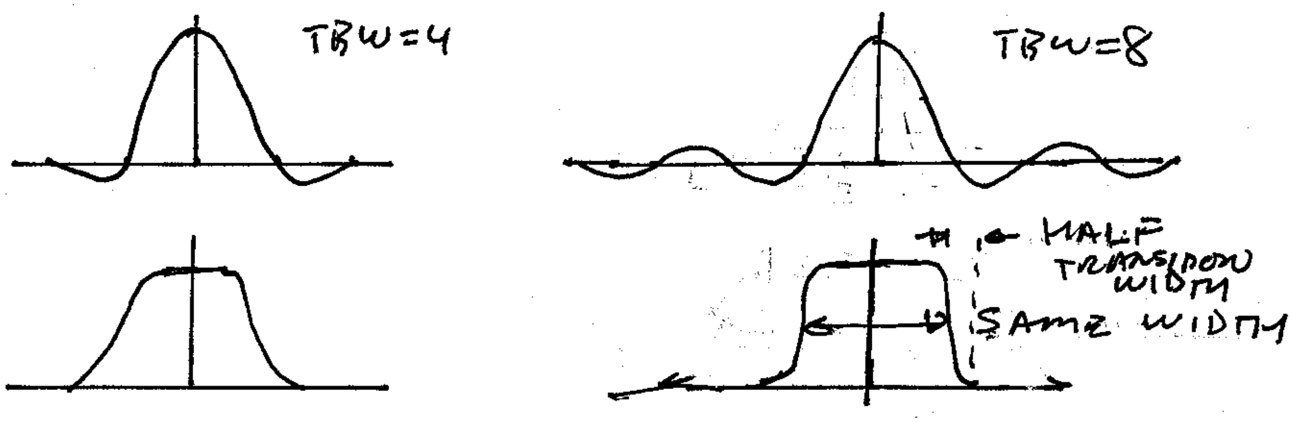
$$= 2N$$ TOTAL NUMBER OF ZEROS

TYPICAL PULSES



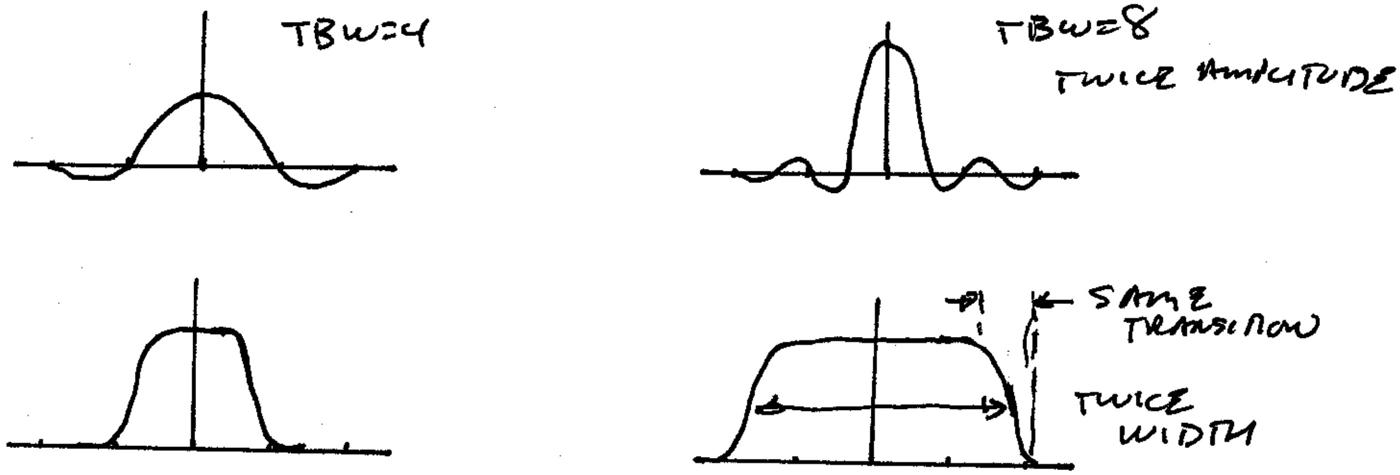
TBW=2	TBW=4	TBW=8	TBW=12
SSFP α's	180°	90°'s α's	SAT PULSES SLAB SELECT
msinc = 1/2	msinc = 1	msinc = 2	msinc = 3

IF WE FIX BANDWIDTH, AND MAKE T LONGER



MORE SELECTIVE PROFILE

IF WE <ins>FIX DURATION</ins>, AND INCREASE BANDWIDTH



WIDER EXCITATION

TYPICALLY IN MR WE <ins>FIX DURATION</ins>, AND <ins>ADJUST THE GRADIENT AMPLITUDE</ins> TO COMPENSATE FOR THE INCREASED BANDWIDTH

EXAMPLE

WE WANT A TBW=8 (msinc 2) PULSE WITH A 2ms DURATION.

IF THE SLICE THICKNESS IS 1cm, WHAT IS THE GRADIENT AMPLITUDE?

ANSWER:

$$(T)(BW) = 8$$
$$(2ms)(BW) = 8$$
$$BW = 4\,kHz$$

WE WANT THIS TO CORRESPOND TO A SLICE THICKNESS $\Delta z = 1\,cm$

$$\frac{\gamma}{2\pi} G \Delta z = 4\,kHz$$

$$(4.257\,kHz/G)\,G\,(1cm) = 4\,kHz$$

$$\underline{\underline{G = 0.94\,G/cm}}$$