

ASSIGNMENT

READ CHAPTER 6

THINK ABOUT PROJECTS

LAST TIME

ADIABATIC INVERSIONS

TODAY

ADIABATIC ROTATIONS

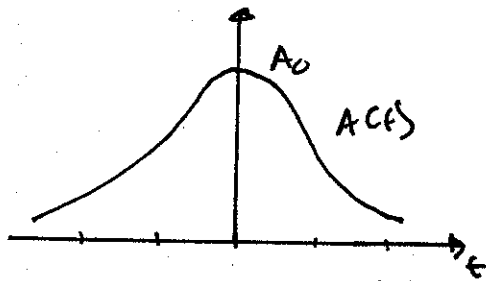
ADIABATIC INVERSIONS: REVIEW

FREQUENCY MODULATED PULSE

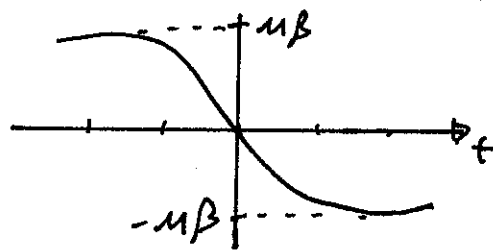
$$\underline{B}_1(t) = A(t) e^{-i\omega_1(t)t}$$

IN ROTATING FRAME AT LARMOR FREQUENCY

TYPICAL WAVEFORMS:



$$A(t) = A_0 \operatorname{sech}(\beta t)$$



$$\omega_1(t) = -M\beta \tanh \beta t$$

MANY OTHER POSSIBILITIES

IN THE ROTATING FRAME AT ω_0

$$\underline{B}(t) = (A(t) \cos \omega_1(t)t, A(t) \sin \omega_1(t)t, 0)$$

IN THE ROTATING FRAME AT $\omega_0 + \omega_1(t)$

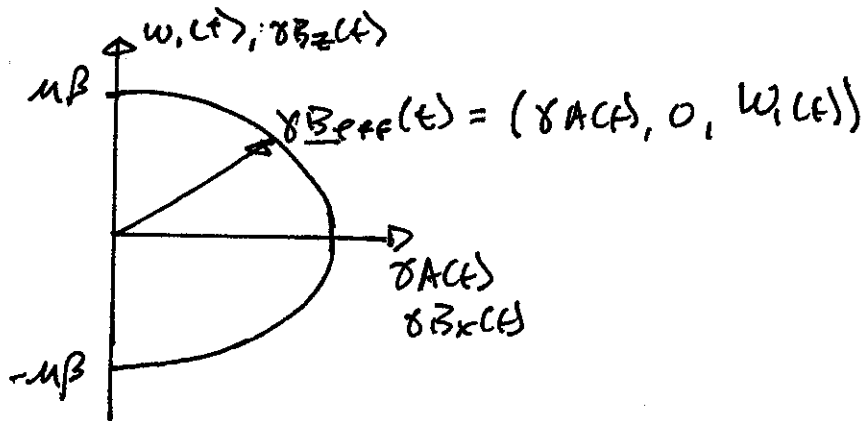
$$\underline{B}_{\text{eff}}(t) = \left(A(t), 0, \frac{\omega_1(t)}{\gamma} \right)$$

FREQUENCY MODULATION OF $\underline{B}_1(t)$ CORRESPONDS

TO \mathcal{E} -FIELD IN ROTATING FRAME AT
MODULATION FREQUENCY.

SWEEP DIAGRAM

PLOT OF $B_{eff}(t)$

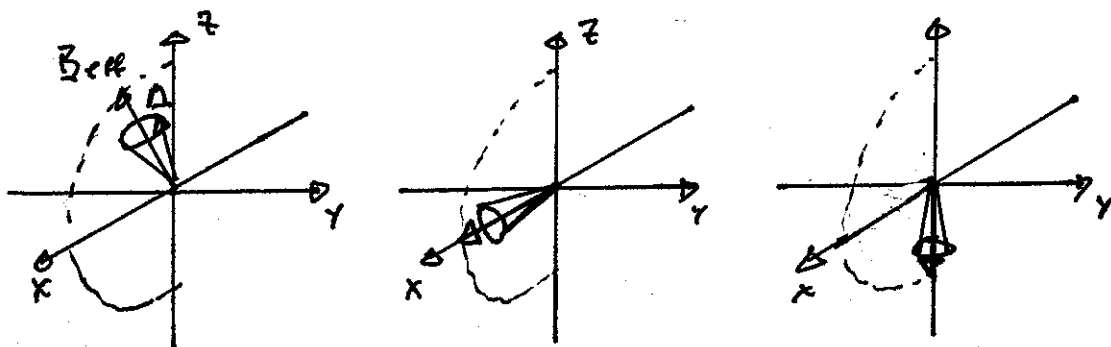


B_eff SWEEP FROM $+z$ TO $-z$

M FOLLOWS, PROVIDED $\psi = \angle B_{eff}(t)$ DOESN'T CHANGE TOO FAST COMPARED TO $|B_{eff}(t)|$

$$\left| \frac{d\psi}{dt} \right| \ll \delta |B_{eff}(t)|$$

ADIABATIC CONDITION.



M TRACKS B_eff(t)

OTHER ADIABATIC PULSES

EXCITATION

SPIN-ECHO

ROTATION BY ARBITRARY ANGLE

EXCITATION

WHY NOT SAVE ADIABATIC INVERSION

TO $\pi/2$?

TWO ANSWERS:

- 1) BELOW ADIABATIC THRESHOLD (i.e. π PULSE)
AN "ADIABATIC" PULSE IS THE SAME AS
ANY OTHER PULSE, WITH

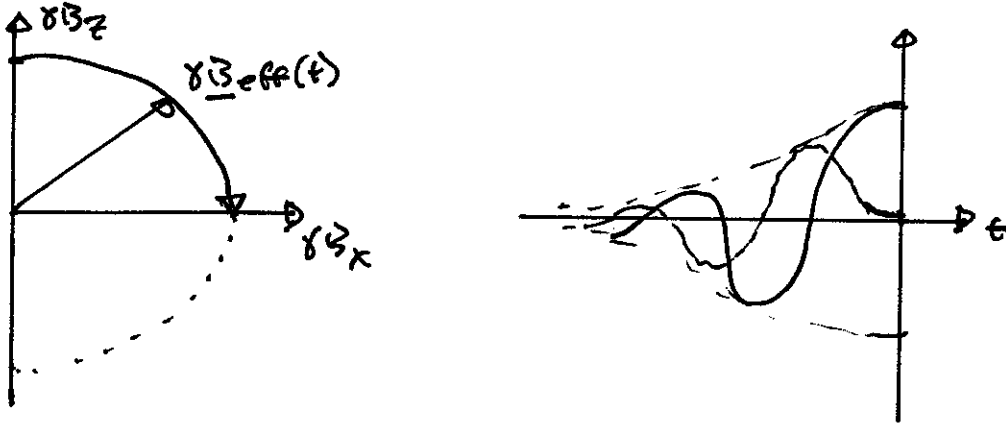
$$\theta = \int_0^T \delta B_1(t) dt$$

WHICH IS NOT B_1 INSENSITIVE

- 2) ADIABATIC PULSES ARE GENERALLY
APPROXIMATELY QUADRATIC PULSES,
DON'T REFOCUS.

SIMPLE ADIABATIC EXECUTION

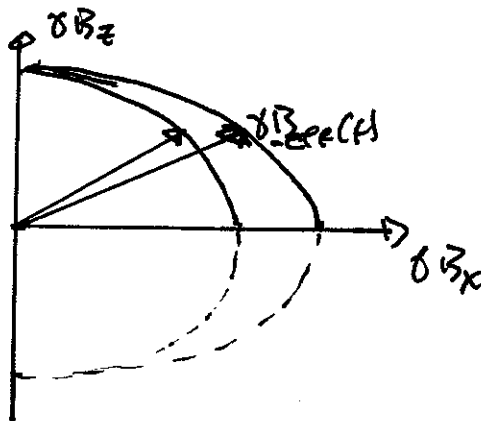
ADIABATIC HALF PASSAGE HALF OF AN
INVERSION SWEEP.



FIRST HALF OF HYPERBOLIC SEICANT

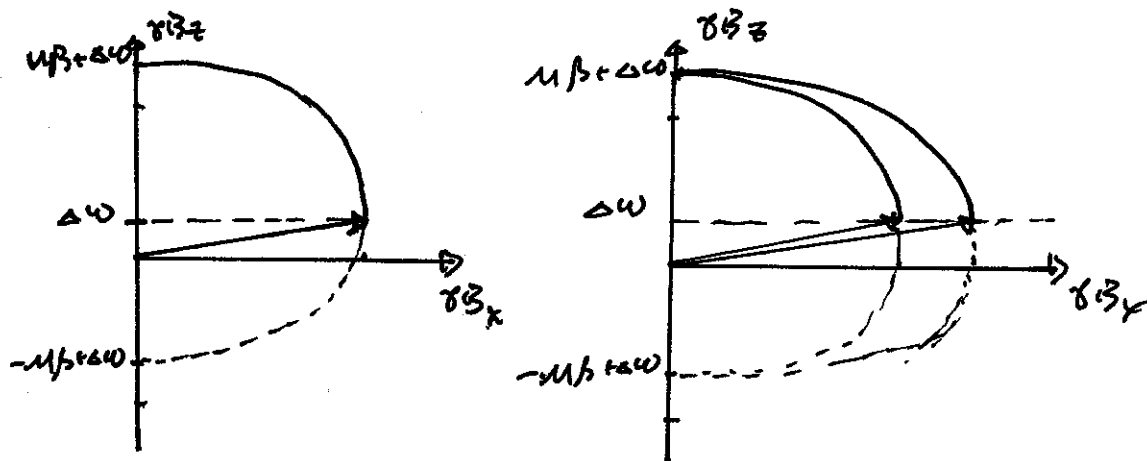
$$\left. \begin{aligned} A(t) &= A_0 \operatorname{sech}(\beta t) \\ W(t) &= -\mu\beta \tanh(\beta t) \end{aligned} \right\} -\infty < t < 0$$

β , INSENSITIVE, ABOVE ADIABATIC THRESHOLD



IN LEFT ALONG +X AXIS

SENSITIVE TO OFF-RESONANCE



OFF-RESONANCE SHIFT OF $\Delta \omega$ LEAVES β_{eff} AND M_z AT AN ANGLE

$$\phi = \tan^{-1} \left(\frac{\Delta \omega}{\gamma A_0} \right)$$

ABOUT THE TRANSVERSE PLANE

ϕ DECREASES AS β_1 INCREASES.

WORKS REASONABLY WELL FOR CREATING M_{xy}
 INSENSITIVE TO ϕ

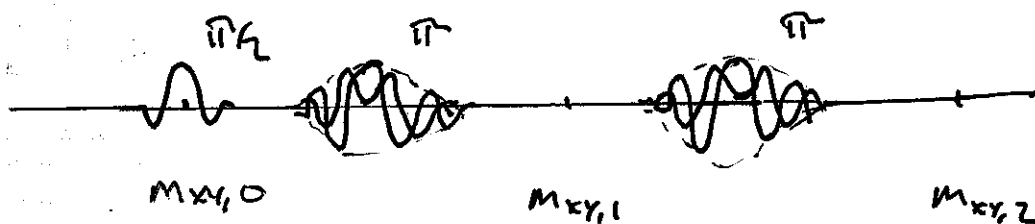
WORKS VERY POORLY FOR ELIMINATING M_z ,
 (i.e. SATURATION PULSES)

ADIABATIC REFocusing PULSES

WHY NOT USE AN ADIABATIC INVERSION?

- 1) ACCURATELY RETURNS TRANSVERSE MAGNETIZATION TO TRANSVERSE PLANE
- 2) ADDS NON-LINEAR PHASE

SIMPLE SOLUTION: USE A PAIR OF ADIABATIC INVERSIONS



THE ADIABATIC π PRODUCES A ROTATION DESCRIBED BY $(\alpha_{\pi}, \beta_{\pi})$

$$M_{xy,1} = (M_{xy,0})^{\psi} \beta_{\pi}^2$$

$$\begin{aligned} M_{xy,2} &= (M_{xy,1})^{\psi} \beta_{\pi}^2 \\ &= ((M_{xy,0})^{\psi} \beta_{\pi}^2)^{\psi} \beta_{\pi}^2 \\ &= M_{xy,0} |\beta_{\pi}|^4 \end{aligned}$$

AS LONG AS WE USE TWO IDENTICAL
REFOCUSING PULSES, PHASE PROFILES
CANCEL.

CHANGES IN B_1 AMPLITUDE WILL
CHANGE β PHASE, BUT DOESN'T MATTER

DISADVANTAGE:

MUST FORM FIRST ECHO

LONGER DELAY UNTIL FIRST USEFUL ECHO,
WHICH IS THE SECOND

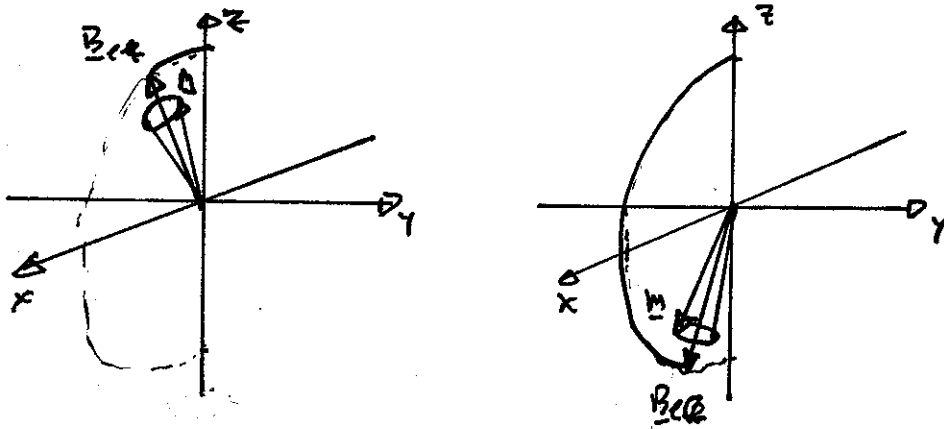
ONLY EVEN ECHOES USABLE

IDEALLY WE WANT A SINGLE PULSE.

BASIC TOOLS FOR ADIABATIC PULSE DESIGN

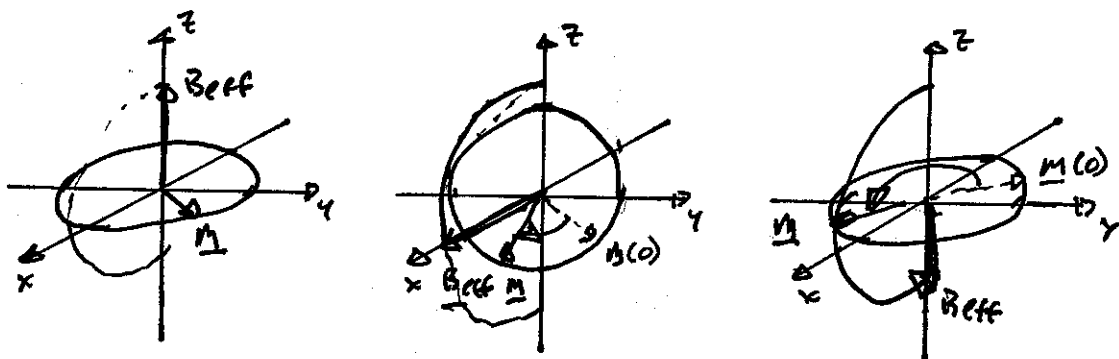
FOR ADIABATIC SWEEPS:

PARALLEL COMPONENT STAYS PARALLEL



THIS IS WHAT WE USE FOR ADIABATIC INVERSION PULSES

PERPENDICULAR COMPONENT STAYS PERPENDICULAR



FOR INITIAL TRANSVERSE MAGNETIZATION

1) INVERTED

2) ADDITIONAL PHASE DUE TO PRECESSION

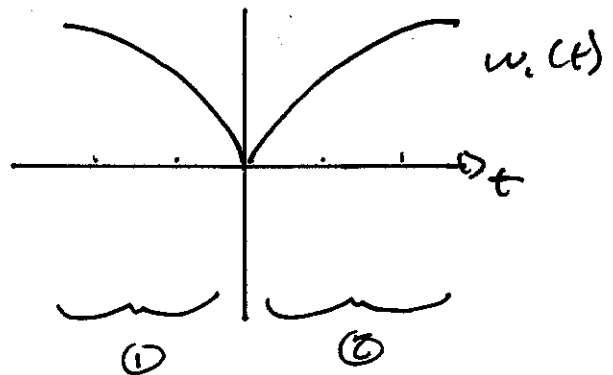
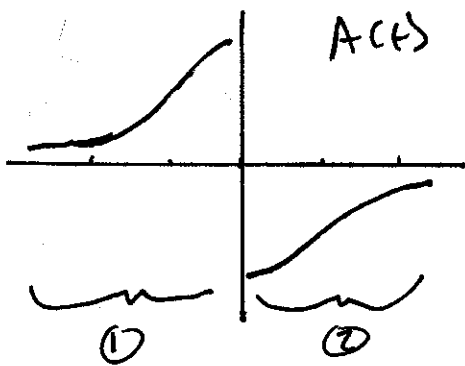
$$\theta_{\text{eff}} = \int_0^T \delta / B_{\text{eff}}(t) dt$$

REFOCUSING PULSES COMBINE PARTIAL SWEEPS
TO DO THE INVERSION WHILE CANCELING
OUT THE PRECESSION PHASE SHIFTS

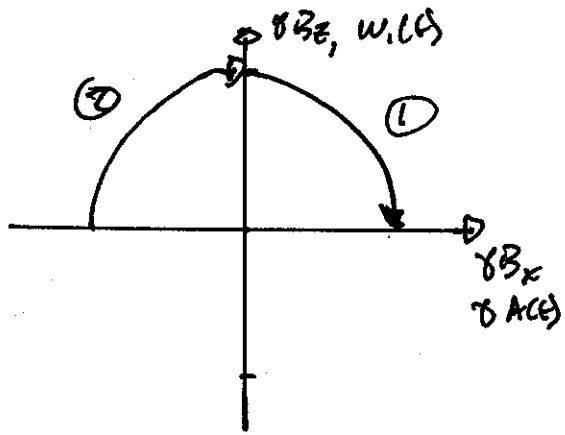
SIMPLE ADIABATIC REFocusing PULSE

β_1 INSENSITIVE REFocusing PULSE - 1 ($\beta_1 \text{ REF} = 1$)

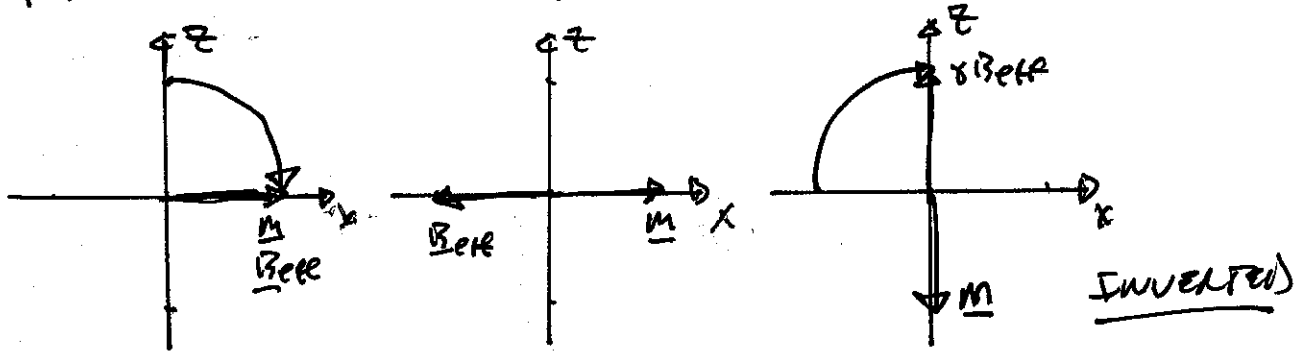
ENVELOPE / MODULATION WAVEFORMS



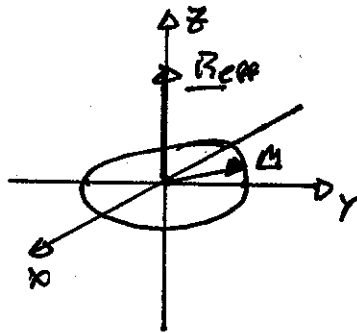
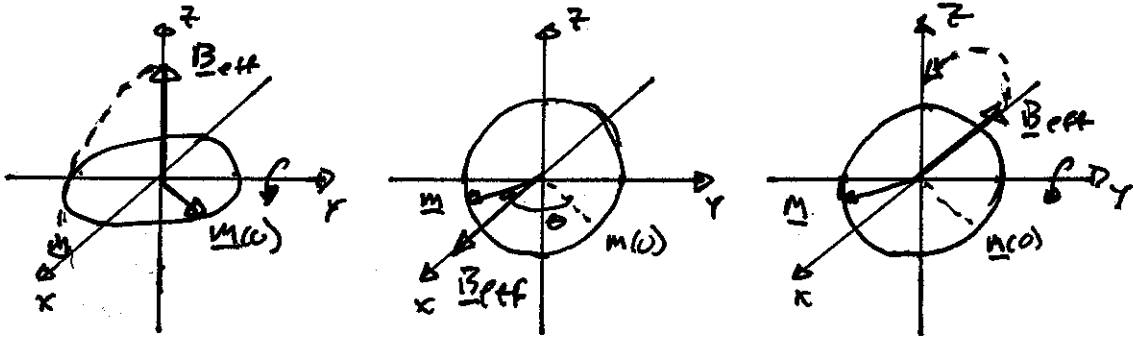
SWEEP DIAGRAM



PARALLEL COMPONENT, INITIALLY ALONG +z



PERPENDICULAR COMPONENT, INITIALLY TRANSVERSE



M HAS BEEN REFLECTED ABOUT xy AXIS!

RESULT IS A SPIN-ECHO PULSE.

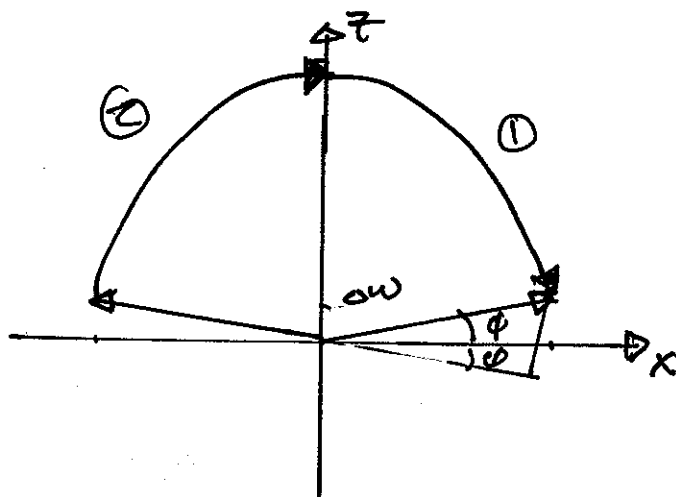
PULSE IS ADIABATIC, BECAUSE IT DEPENDS ONLY ON THE SWEEP

B_1 AMPLITUDE ONLY EFFECTS

$$\theta_{eff} = \int_{-\infty}^0 |B_{eff}(t)| dt$$

WHICH CANCELS OUT AT END.

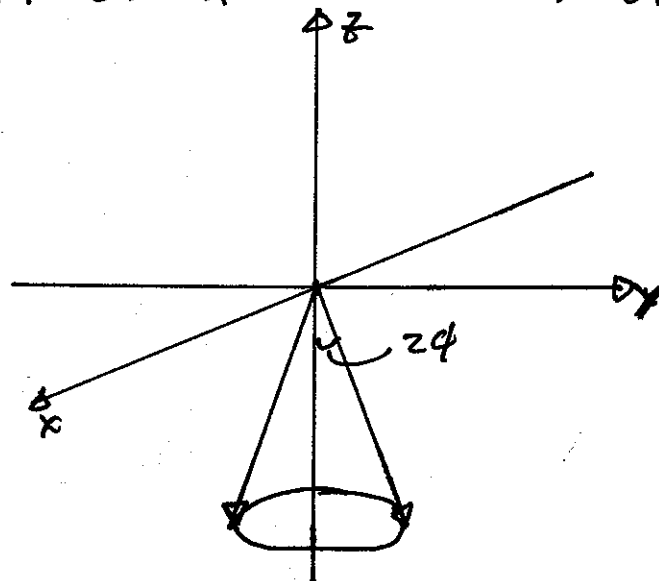
OFF-RESONANCE SENSITIVITY



$$\phi = \tan^{-1}\left(\frac{\Delta\omega}{\delta A_0}\right)$$

AFTER SIGN CHANGE, PARALLEL COMPONENT TRACKS, PERPENDICULAR COMPONENT TRACKS AND PRECESSES.

RESULT IS INITIAL MAGNETIZATION ALONG z IS LEFT ON A CONE OF ANGLE $\pm 2\phi$



SIMILAR PROBLEM FOR TRANSVERSE COMPONENT.

ADIABATIC ROTATION PULSES

ROTATION BY SOME ARBITRARY ANGLE

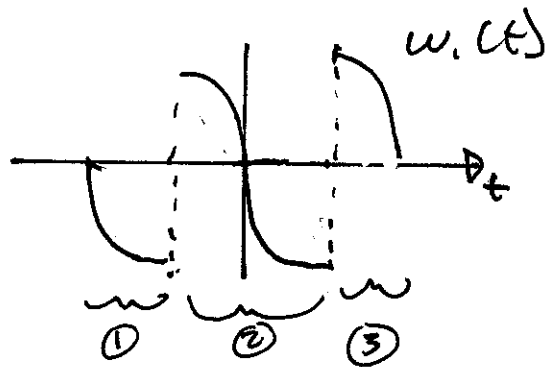
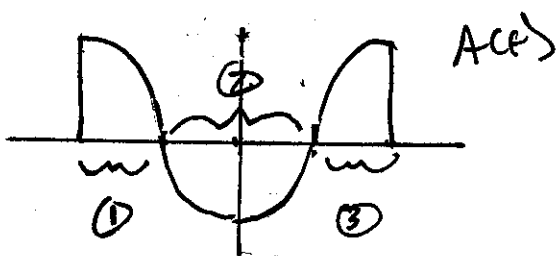
SMALL π P ANGLE

$\pi/2$ EXCITATION / SATURATION

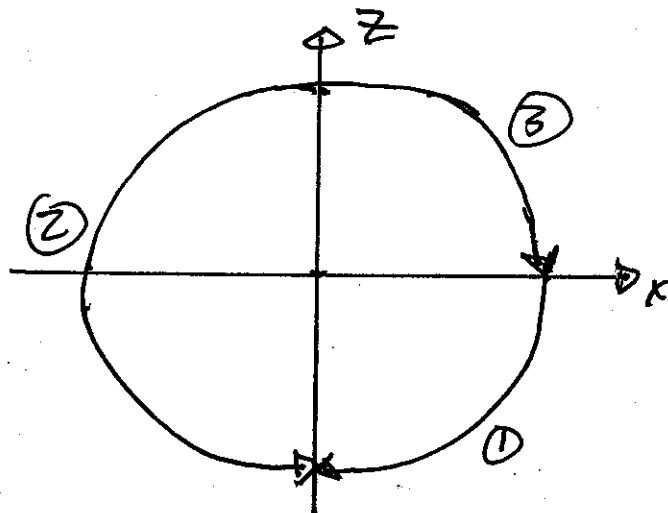
SPIN-ECHO REFocusing PULSE

B₁ SENSITIVE ROTATION - 4 (BIR-4)

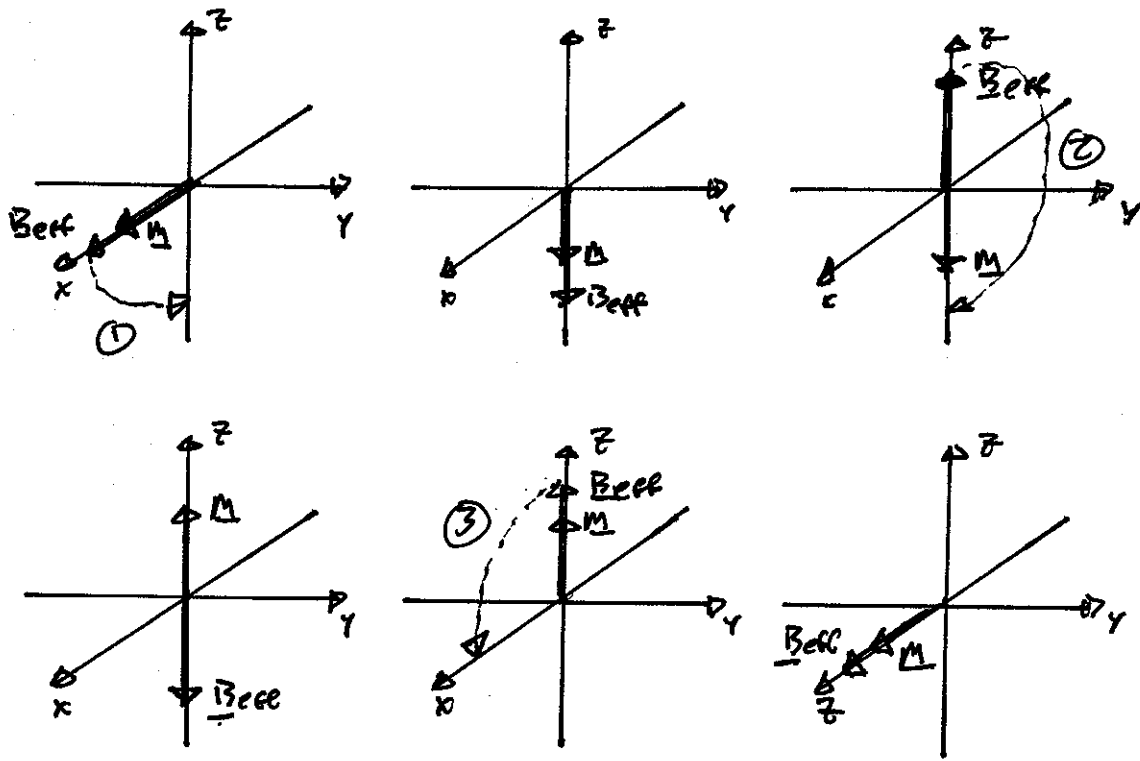
ENVELOPE / MODULATION WAVEFORMS



SWEEP DIAGRAM



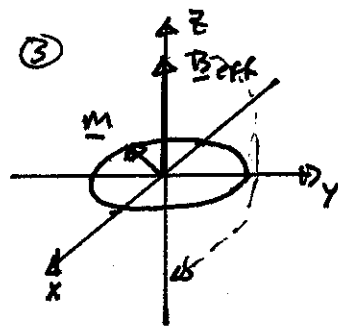
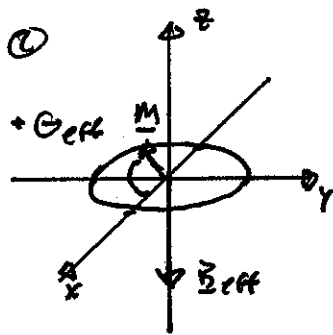
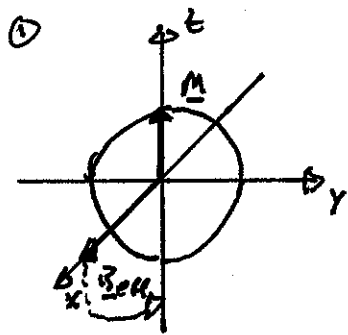
SPIN INITIALLY ALONG $+x$, PARALLEL



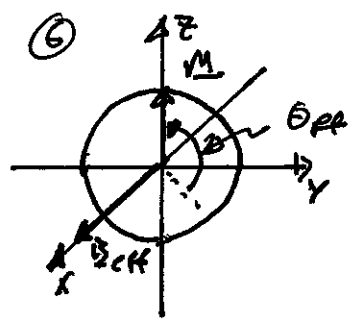
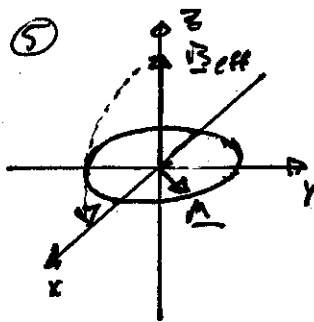
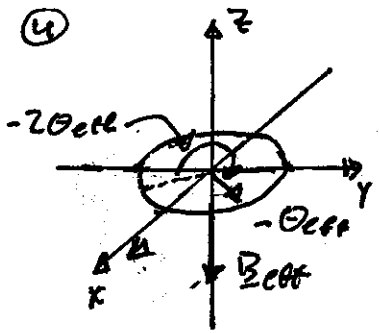
RETURNS M TO $+x$

DOES NOTHING!

SPIN INITIALLY PERPENDICULAR (+z, FOR EXAMPLE)



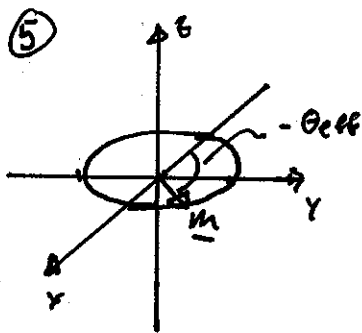
$\theta_{eff} = \text{PHASE OF HALF SWEEP}$



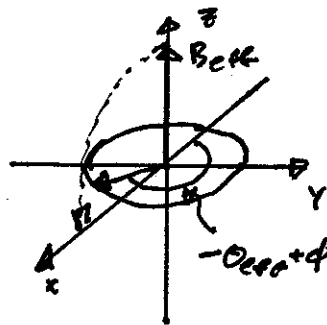
RETURNS M TO +z

DOES NOTHING!

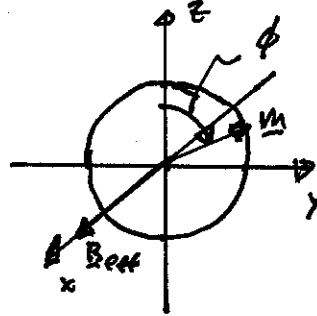
KEY IDEA: ADD PHASE SHIFT IN RF
BEFORE FINAL SWEEP



PREPHASED BY
 $-\theta_{eff}$



PHASE SHIFT
BY ϕ



$-\theta_{eff}$ CANCELED
LEFT WITH ϕ

ROTATION BY ϕ ABOUT THE $+x$ AXIS!

PHASE SHIFT IS VERY ACCURATE.

\Rightarrow VERY ACCURATE ROTATION

ANY ANGLE POSSIBLE

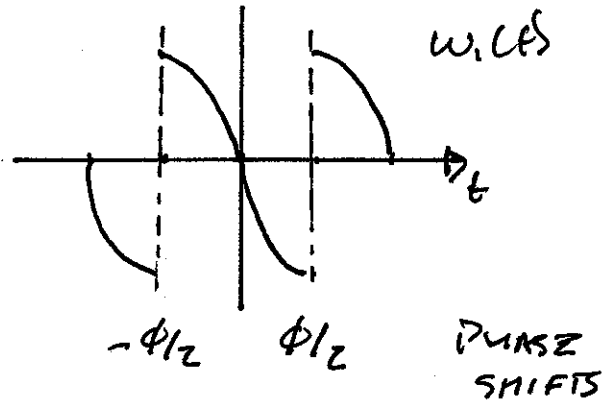
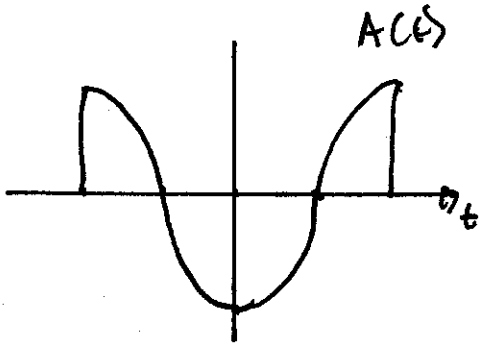
SMALL TIP (i.e. 30°)

EXCITATION (90°)

REFOCUSING (180°)

ALL HAVE SAME POWER

BETTER APPROACH: SPLIT PHASE SHIFT
OVER BOTH JUMPS



BIR-4