

Task Control

Unified Motion/Force Control

$F = F_{motion} + F_{contact}$

Unified Motion/Force Control

- Generalized Selection Matrix
- Dynamic Model (Homogeneity)

$$\Lambda_0(x) \dot{\vartheta} + \mu_o(x, \vartheta) + p_0(x) + F_{contact} = F_0$$

Task Description

Task Specification

$$F = \Sigma F_{motion} + \bar{\Sigma} F_{force}$$

Selection matrix

$$\Sigma = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix}; \bar{\Sigma} = I - \Sigma$$

Generalized Selection Matrix

$$f_{(R_f)} = S_f f_{(R_0)}$$

Selection in R_f

$$\bar{\Sigma} f_{R_f}$$

Selection in R_0

$$S_f^T \bar{\Sigma} S_f f_{R_0} \leftarrow S_f^T \bar{\Sigma} f_{R_f}$$

Generalized Selection Matrix

$$\Sigma_F = \begin{pmatrix} \sigma_{F_x} & 0 & 0 \\ 0 & \sigma_{F_y} & 0 \\ 0 & 0 & \sigma_{F_z} \end{pmatrix}; \quad \bar{\Sigma}_F = I_3 - \Sigma_F$$

$$\Sigma_M = \begin{pmatrix} \sigma_{M_x} & 0 & 0 \\ 0 & \sigma_{M_y} & 0 \\ 0 & 0 & \sigma_{M_z} \end{pmatrix}; \quad \bar{\Sigma}_M = I_3 - \Sigma_M$$

Generalized Selection Matrix

$$\Omega = \begin{pmatrix} S_F^T \Sigma_F S_F & 0 \\ 0 & S_M^T \Sigma_M S_M \end{pmatrix}$$

$$\bar{\Omega} = \begin{pmatrix} S_F^T \bar{\Sigma}_F S_F & 0 \\ 0 & S_M^T \bar{\Sigma}_M S_M \end{pmatrix}$$

Basic Dynamic Model

Operational force $\stackrel{?}{\equiv}$ Forces & Moments

$$\dot{X} = J(q)\dot{q}$$

$$\Gamma = J^T(q)F$$

Forces & Moments

$$\begin{pmatrix} v \\ \omega \end{pmatrix} = J_0(q)\dot{q} \quad \begin{aligned} J\dot{q} &= E(X)J_0\dot{q} \\ \dot{X} &= E \begin{pmatrix} v \\ \omega \end{pmatrix} \end{aligned}$$

$$F_0 \doteq \begin{pmatrix} f \\ m \end{pmatrix}; \quad \begin{aligned} J^T F &= J_0^T E^T F \\ \begin{pmatrix} f \\ m \end{pmatrix} &= E^T F \end{aligned}$$

Basic Dynamic Model

$$\Lambda_0 = E^T \Lambda E$$

$$\Lambda \ddot{x} + \mu(x, \dot{x}) + p(x) = F$$

$$\Downarrow E^T$$

$$\Lambda_0 \ddot{\vartheta} + \mu_0(x, \vartheta) + p_0(x) = F_0$$

with $\vartheta \doteq \begin{pmatrix} v \\ \omega \end{pmatrix}$

Orientation Representation

$$\begin{matrix} x_r \\ x_{rd} \end{matrix} \rightarrow \delta x_r = x_r - x_{rd}$$

$$\dot{x}_r = E_r \omega$$

Instantaneous Angular Error

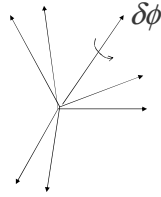
$$\delta x_r = E_r \delta \phi$$

Instantaneous Angular Error

$$\dot{x}_r = E_r \omega$$

$$\delta x_r = E_r \delta \phi$$

$$\delta \phi = E_r^+ \delta x_r$$



Control - Position Errors

$$(x - x_d) = \begin{pmatrix} x_p - x_{pd} \\ x_r - x_{rd} \end{pmatrix}$$

$$\begin{matrix} \dot{x}_r = E_r \omega \\ \delta x_r = E_r \delta \phi \end{matrix} \Rightarrow \begin{pmatrix} x_p - x_{pd} \\ \delta \phi \end{pmatrix} \text{ Error Vector}$$

$$\delta x_r = (x_r - x_{r(d)}) = E_r \delta \phi$$

$$\delta \phi = E_r^+ (x_r - x_{r(d)})$$

Goal Position

$$x_d = \begin{bmatrix} x_{pd} \\ x_{rd} \end{bmatrix}$$

$$f^* = -k_p (x_p - x_{pd}) - k_v \dot{x}_p$$

$$m^* = -k_p \delta \phi - k_v \omega$$

$$\text{with } \delta \phi = E_r^+ (x_r - x_{rd})$$

Closed loop

$$I \ddot{x}_p + k_v \dot{x}_p + k_p (x_p - x_{pd}) = 0$$

$$I \dot{\omega} + k_v \omega + k_p \delta \phi = 0$$

Direction Cosines

$$\mathbf{x}_r = (S_1^T S_2^T S_3^T)^T$$

$$\mathbf{x}_{rd} = (S_{1d}^T S_{2d}^T S_{3d}^T)^T$$

$$E_r^+ = \frac{1}{2} E_r^T$$

$$\text{where } E_r^T(\mathbf{x}_r) = \begin{pmatrix} -\hat{S}_1^T & -\hat{S}_2^T & -\hat{S}_3^T \end{pmatrix}$$

$$\delta \Phi = \frac{1}{2} E_r^+(\mathbf{x}_r)(\mathbf{x}_r - \mathbf{x}_{rd})$$

$$\delta X_r = \begin{bmatrix} S_1 - S_{1d} \\ S_2 - S_{2d} \\ S_3 - S_{3d} \end{bmatrix} = \begin{bmatrix} S_1 \\ S_2 \\ S_3 \end{bmatrix} - \begin{bmatrix} S_{1d} \\ S_{2d} \\ S_{3d} \end{bmatrix}$$

since

$$E_r^T(\mathbf{x}_r)\mathbf{x}_r = \hat{S}_1 S_1 + \hat{S}_2 S_2 + \hat{S}_3 S_3 = 0$$

The angular rotation error

$$\delta \Phi = -\frac{1}{2} (\hat{S}_1 S_{1d} + \hat{S}_2 S_{2d} + \hat{S}_3 S_{3d})$$

Euler Parameters

The end-effector orientation

$$\mathbf{x}_r = \lambda = (\lambda_0 \lambda_1 \lambda_2 \lambda_3)^T$$

The desired orientation

$$\lambda_d = (\lambda_{0d} \lambda_{1d} \lambda_{2d} \lambda_{3d})^T$$

The orientation error vector

$$\delta \lambda = \lambda - \lambda_d$$

The left inverse

$$E_r^+(\mathbf{x}_r) = 2 \overset{\vee}{\lambda}^T$$

where

$$\overset{\vee}{\lambda} = \begin{pmatrix} -\lambda_1 & \lambda_0 & -\lambda_3 & \lambda_2 \\ -\lambda_2 & \lambda_3 & \lambda_0 & -\lambda_1 \\ -\lambda_3 & -\lambda_2 & \lambda_1 & \lambda_0 \end{pmatrix}$$

Noting that

$$\overset{\vee}{\lambda} \lambda = 0$$

The angular rotation error

$$\delta \Phi = -2 \overset{\vee}{\lambda} \lambda_d$$

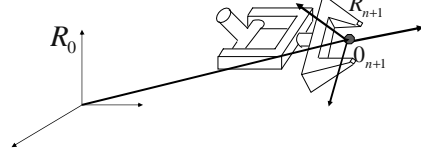
Angular Acceleration

$$\dot{X}_r = E_r \omega$$

$$\ddot{X}_r = E_r \dot{\omega} + \dot{E}_r \omega$$

$$\dot{\omega} = E_r^+ \ddot{X}_r - \dot{E}_r^+ \omega$$

Acceleration Direction Cosines



The orientation is described by

$$\mathbf{x}_r = (S_1^T S_2^T S_3^T)^T$$

$$S1 = x_{(n+1)}; S2 = y_{(n+1)}; S3 = z_{(n+1)};$$

The second time derivatives

$$\frac{d^2 \mathbf{x}_{(n+1)}}{dt^2} = -\mathbf{x}_{(n+1)} \times \dot{\omega} + (\mathbf{x}_{(n+1)} \times \omega) \times \omega$$

$$\frac{d^2 \mathbf{y}_{(n+1)}}{dt^2} = -\mathbf{y}_{(n+1)} \times \dot{\omega} + (\mathbf{y}_{(n+1)} \times \omega) \times \omega$$

$$\frac{d^2 \mathbf{z}_{(n+1)}}{dt^2} = -\mathbf{z}_{(n+1)} \times \dot{\omega} + (\mathbf{z}_{(n+1)} \times \omega) \times \omega$$

However

$$\mathbf{u} \times \mathbf{v} \times \mathbf{w} = (\mathbf{u}^T \mathbf{v}) \mathbf{w} - (\mathbf{v}^T \mathbf{w}) \mathbf{u}$$

This yields

$$\ddot{\mathbf{x}}_r = E(\mathbf{x}_r) \dot{\omega} + R(\mathbf{x}_r, \omega) \omega - (\omega^T \omega) \mathbf{x}_r$$

where

$$R(\mathbf{x}_r, \omega) = \begin{pmatrix} (S_1^T \omega) I_3 \\ (S_2^T \omega) I_3 \\ (S_3^T \omega) I_3 \end{pmatrix}$$

Acceleration Direction Cosines

$$\dot{\omega}_d = \frac{1}{2} E^T \ddot{x}_{rd} + \frac{1}{2} R^T(x_r, \omega) \dot{x}_{rd}$$

Euler Parameters

The acceleration associated with Euler parameters

$$\ddot{\lambda} = \frac{1}{4} \overset{\vee}{\lambda} \dot{\omega} - \frac{1}{2} (\omega^T \omega) \lambda$$

since $\overset{\vee}{\lambda} \lambda = 0$

Euler Parameters

The angular acceleration vector

$$\dot{\omega} = 4 \overset{\vee}{\lambda} \ddot{\lambda}$$

The desired angular acceleration

$$\dot{\omega}_d = 4 \overset{\vee}{\lambda}_d \ddot{\lambda}_d$$

Motion Tracking $(x_{pd}, \dot{x}_{pd}, \ddot{x}_{pd})$

$$F^* = \ddot{x}_{pd} - k_p (x_p - x_{pd}) - k_v (\dot{x}_p - \dot{x}_{pd})$$

Closed loop

$$I \ddot{\epsilon}_x + k_v \dot{\epsilon}_x + k_p \epsilon_x = 0$$

with

$$\epsilon_{x_p} = x_p - x_{pd}$$

Motion Tracking $(x_{pd}, \dot{x}_{pd}, \ddot{x}_{pd})$

$$f^* = \ddot{x}_{pd} - k_p (x_p - x_{pd}) - k_v (\dot{x}_p - \dot{x}_{pd})$$

$$m^* = \dot{\omega}_d - k_p \delta\phi - k_v (\omega - \omega_d)$$

with $\delta\phi = E_r^+ (x_r - x_{rd})$

$$\omega_d = E_r^+ (x_{rd}) \dot{x}_{rd}$$

and

$$\dot{\omega}_d = E_r^+ (x_{rd}) \ddot{x}_{rd} - E_r^+ (x_{rd}) \dot{E}(x_{rd}) \omega_d$$

Closed loop

$$(\ddot{x}_p - \ddot{x}_{pd}) + k_v (\dot{x}_p - \dot{x}_{pd}) + k_p (x_p - x_{pd}) = 0$$

$$(\dot{\omega} - \dot{\omega}_d) + k_v (\omega - \omega_d) + k_p \delta\phi = 0$$

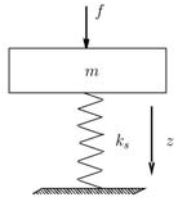
A Mass Spring System

System

$$m\ddot{z} + k_s z = f$$

$$f_s = k_s z$$

$$m \frac{1}{k_s} \ddot{f}_s + f_s = f$$



System
$$m \frac{1}{k_s} \ddot{f}_s + f_s = f$$

Control

$$f = f_s + m \cdot f_{comp}$$

$$f = f_s - m \left[k_f (f_s - f_d) + k_{v_f} \dot{f}_s \right]$$

Control-loop System

$$\ddot{f}_s + k_s k_{v_f} \dot{f}_s + k_s k_f (f_s - f_d) = 0$$

Static Equilibrium

$$f_s = f_d$$

End-Effector/Sensor System

$$\Lambda_0 \dot{\vartheta} + \mu_0(x, \vartheta) + p_0(x) + F_{contact} = F_0$$

Unified Control

$$F_0 = F_{motion} + F_{force}$$

$$F_{motion} = \hat{\Lambda}_0 \Omega F_{motion}^* + \hat{\mu}_0 + \hat{P}_0$$

$$F_{force} = \hat{\Lambda}_0 \bar{\Omega} F_{force}^* + F_{sensor}$$

End-Effector/Sensor System

$$\Lambda_0 \dot{\vartheta} + \mu_0(x, \vartheta) + p_0(x) + F_{contact} = F_0$$

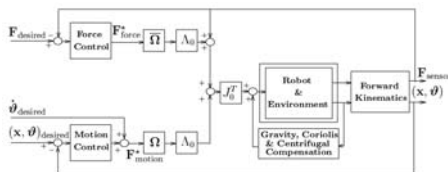
Unified Control

$$F_0 = F_{motion} + F_{force}$$

$$F_{motion} = \hat{\Lambda}_0 \Omega F_{motion}^* + \hat{\mu}_0 + \hat{P}_0$$

$$F_{force} = \hat{\Lambda}_0 \bar{\Omega} F_{force}^* + \bar{\Omega} F_{desired}$$

Unified Motion & Force Control



Two decoupled Subsystems

$$\Omega \dot{\vartheta} = \Omega F_{motion}^*$$

$$\bar{\Omega} \dot{\vartheta} = \bar{\Omega} F_{force}^*$$